



A Practical Sub-synchronous Oscillation in an Offshore Wind Power Plant: Modelling, Analysis and Validation

Lei Shuai, Aalborg, Dec., 05th, 2018

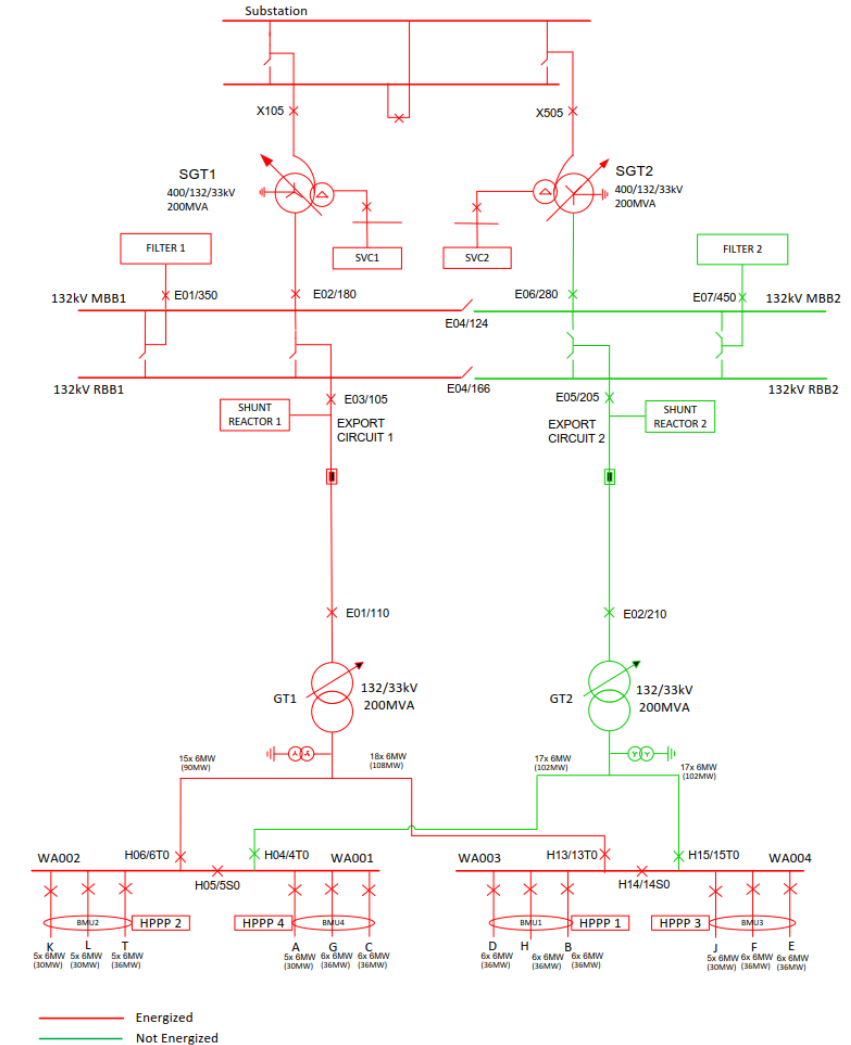
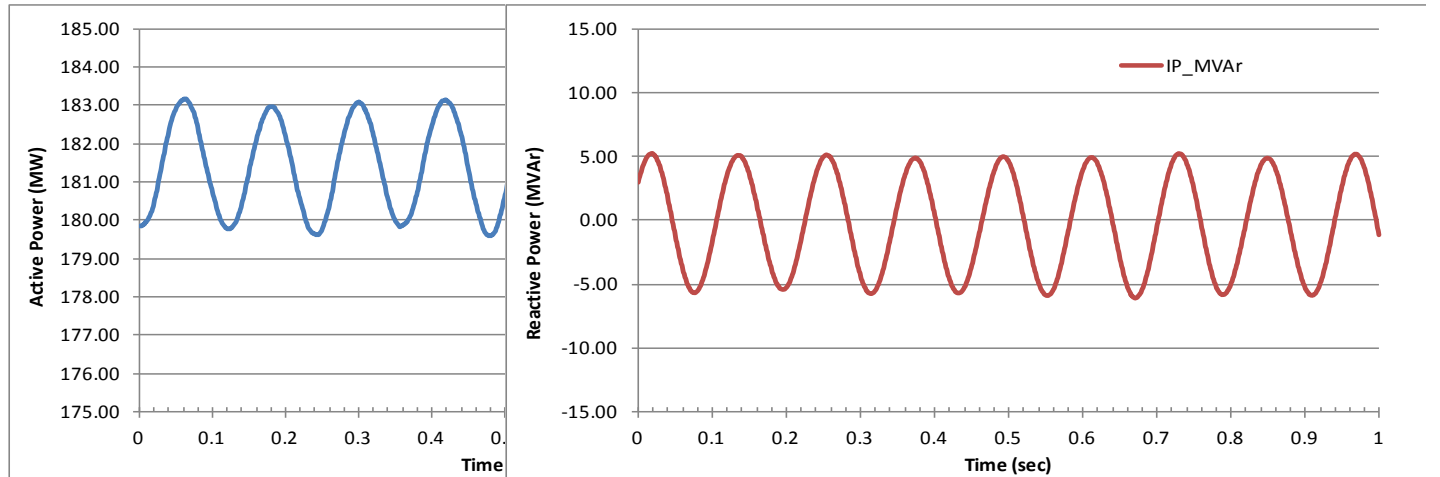
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Introduction

Sub-synchronous Oscillation in an Offshore Wind Power Plant

- 67 SWT-6.0MW turbines, total capacity 402MW
- Stable during all normal operations
- Contingency operation when 1 of 2 HV exporting cables was in service
 - Extremely weak grid with 1.2~1.5 SCR at MV turbine
 - Sub-synchronous oscillation starts when the WPP produces more than 140MW
 - Oscillation frequency was around 8.5Hz



Small-signal stability of power converter-based Power systems

Frequency-Domain Model (FDM) based Stability Approach

- Admittance/Impedance-based approach
- Nyquist stability criterion
- Easy to understand and use, require less information about the system
- Difficult to reveal the root causes of system instability and therefore limited information for control systems tuning

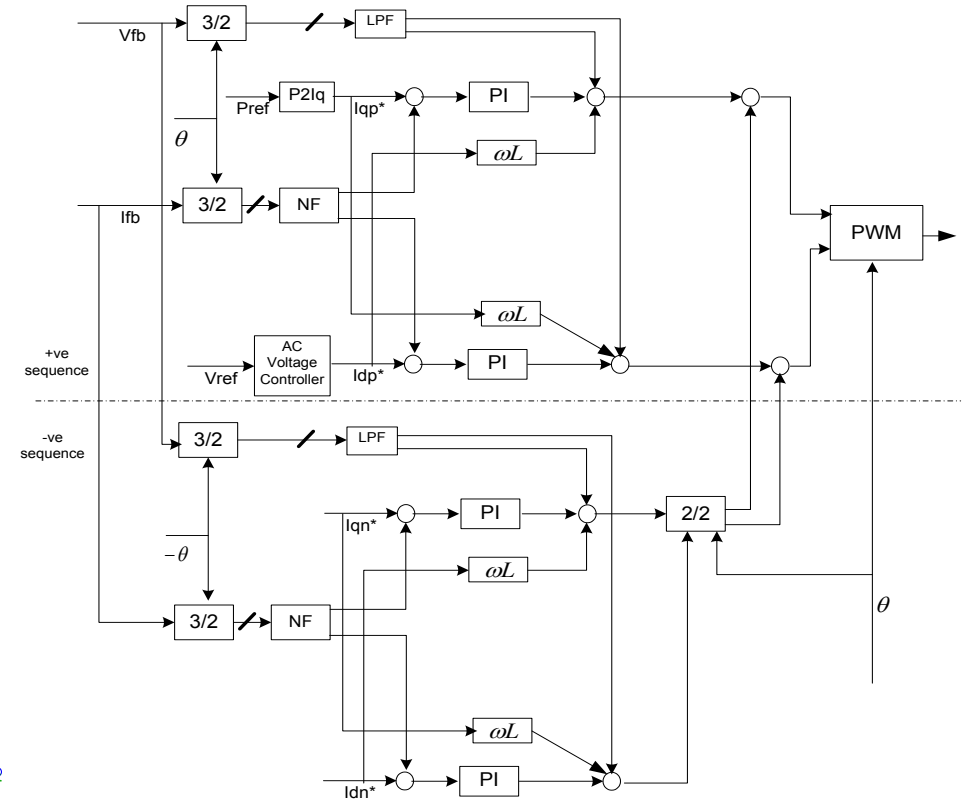
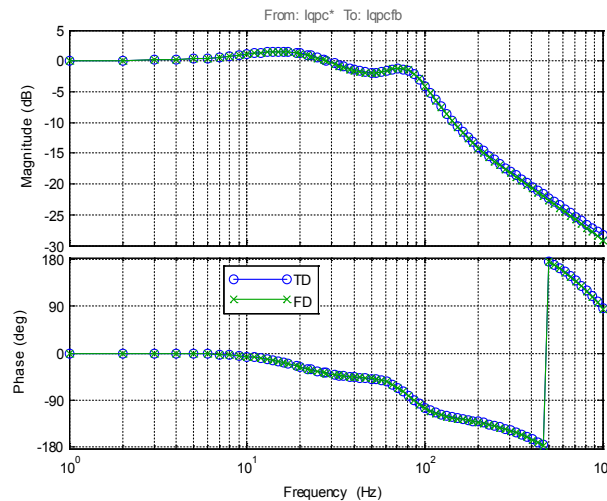
State-space Representation (SSR) based Stability Approach

- Closed-loop study approach, Eigenvalue analysis
- Lyapunov Stability Theory: there is always a stability region around the equilibrium for a stable small-signal linearized system
- LTI system is stable if and only if all the eigenvalues of state matrix of closed-loop system are located in Left Half Plane (LHP)
- Possibility to reveal the relationship of control states and stability of the system
- Require comprehensive information about the control systems and system parameters which are not always easy to obtain

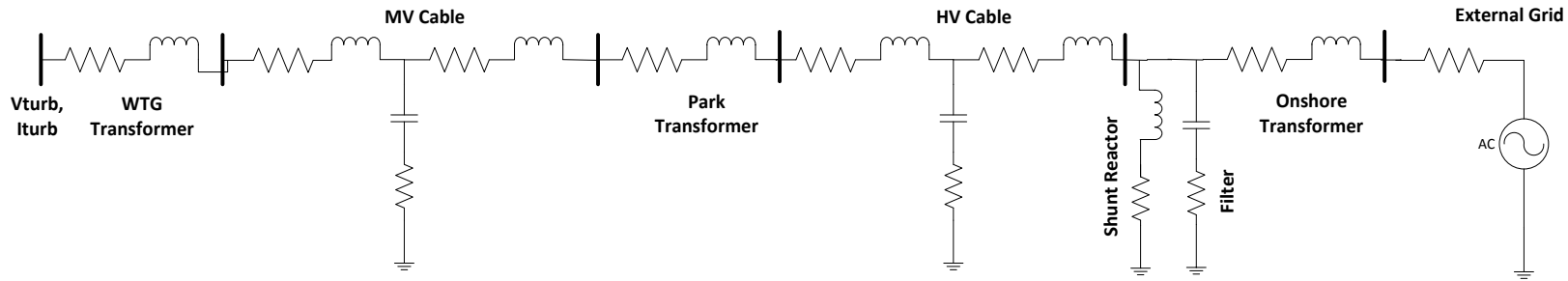
State-space Representation Modelling

Modelling of Net-side VSC in SSR

- A dual feedback control loops: positive and negative sequence control.
- Outer loops are active power control and voltage control.
- DQ Synchronous Rotating Frame (SRF) implementation is employed to mimic the actual design of power converter control.
- Small-signal behavior of PLL is included and modelled to precisely replicate sub-synchronous dynamic of small-signal stability.
- All actual delays including PWM delay, S&H delays, LPFs, Notch filters are included.
- The Net-side VSC model in DQ SRF has been benchmarked against Full Order Model in Time Domain (FOM TD).



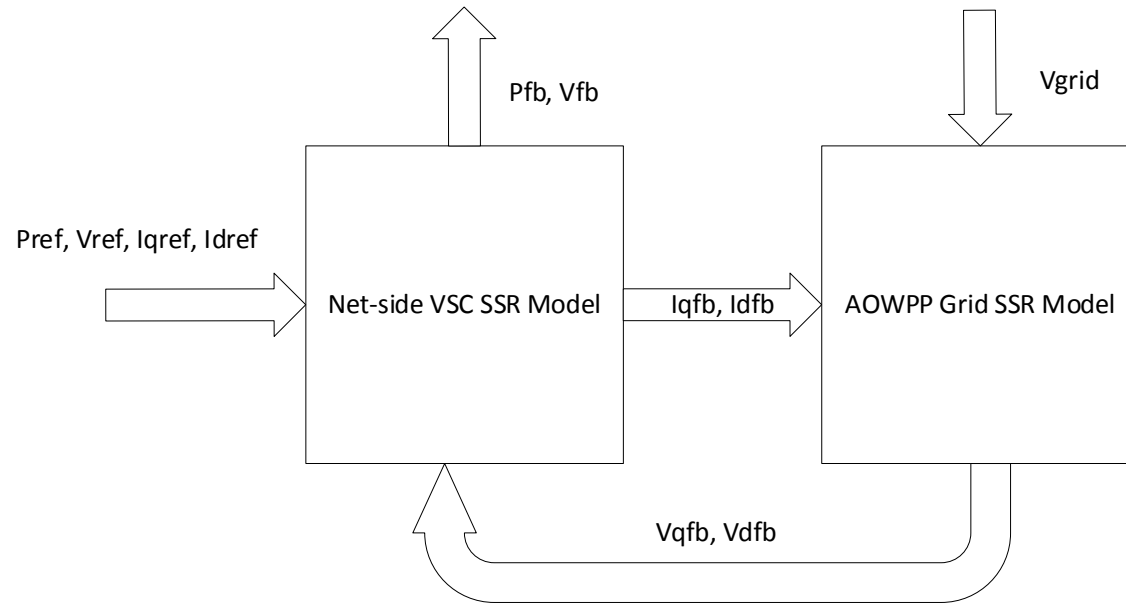
Modelling of AOWPP Grid in SSR



- Supplier's data are used to construct models of electrical components.
- External Grid is modelled as the Thevenion equivalent based on short-circuit capacity provided by TSO.
- AOWPP Grid is modelled in grid SRF to conveniently integrate with Net-side VSC DQ SRF model.
- PLL ensures the frame alignment between grid SRF and DQ SRF.

Integraton of Net-side VSC Model and AOWPP Grid Model

- Both parts are modelled in Matlab as state-space matrix representation (SSR).
- Interconnection interface is defined at LV side of wind turbine transformer.
- A steady state power flow calculator is used to define the operation points based on inputs as Pref, Vref, Vgrid.
- A complete closed-loop system SSR SRF model is formed for stability analysis.



$$\begin{bmatrix} \dot{X} \end{bmatrix} = A[X] + B \begin{bmatrix} P_{ref} \\ V_{ref} \\ Iq_{ref} \\ Id_{ref} \\ \dots \end{bmatrix}$$

$$\begin{bmatrix} P_{fb} \\ V_{fb} \\ Iq_{fb} \\ Id_{fb} \\ \dots \end{bmatrix} = C[X] + D \begin{bmatrix} P_{ref} \\ V_{ref} \\ Iq_{ref} \\ Id_{ref} \\ \dots \end{bmatrix}$$

Site Oscillation Replication in Simulations

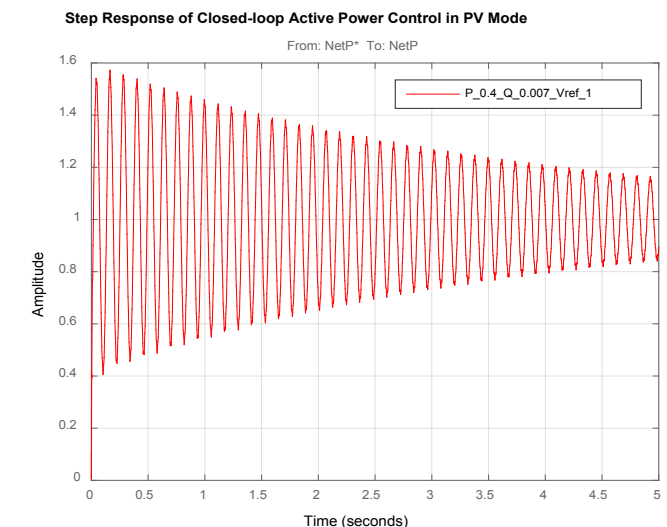
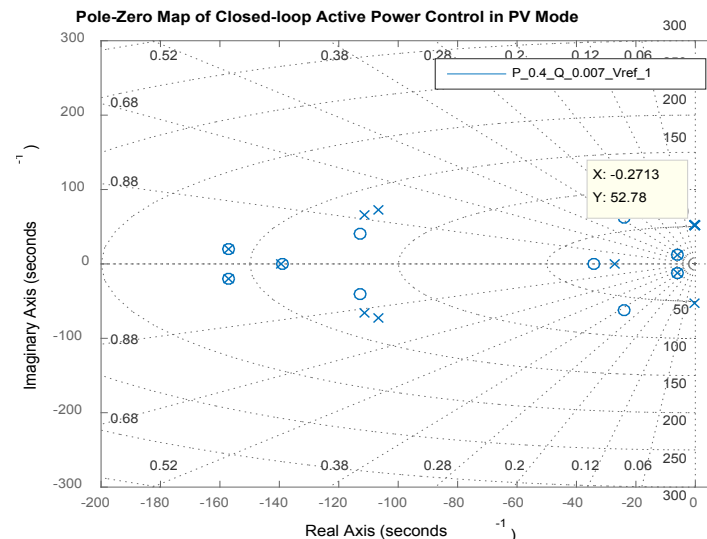
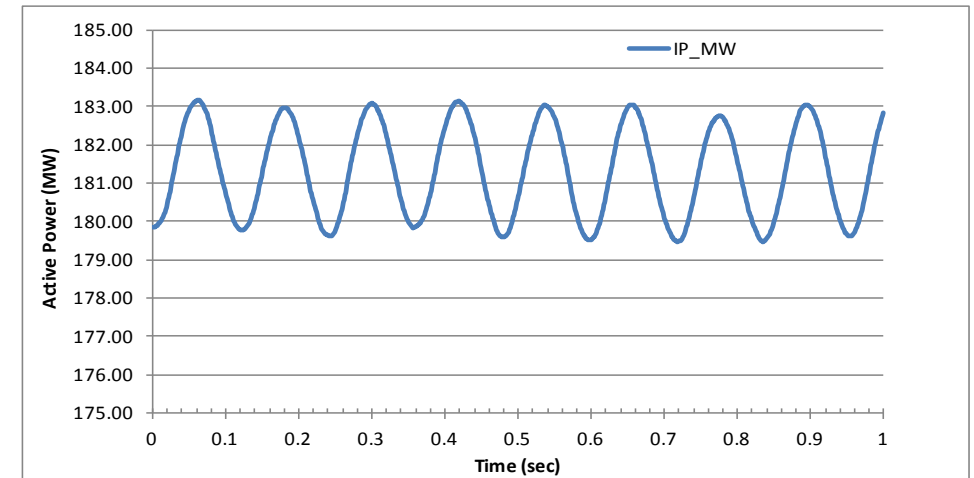
Site Oscillation Replication in Simulations (1/2)

Facts of Site Oscillation

- Contingency operation: single exporting-cable operation
- SCR at MV terminal of turbine transformer reduces to 1.2~1.5
- Appx. 60 WTs were in operation
- Sub-synchronous oscillation started to build up when total power export exceeded 140MW, resulting in each WT producing appx. 40% of rated power
- The oscillation frequency was around 8.5Hz

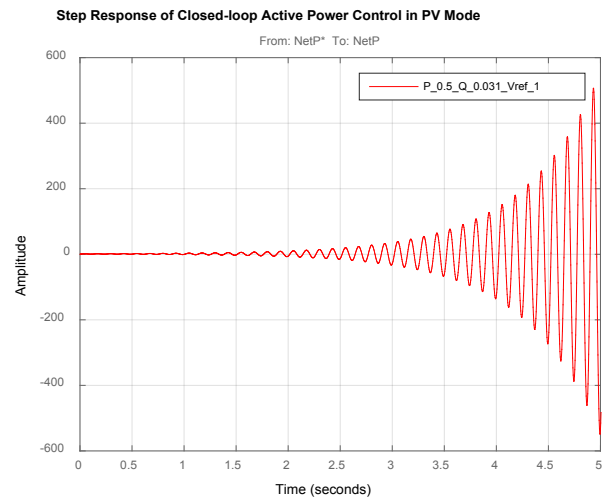
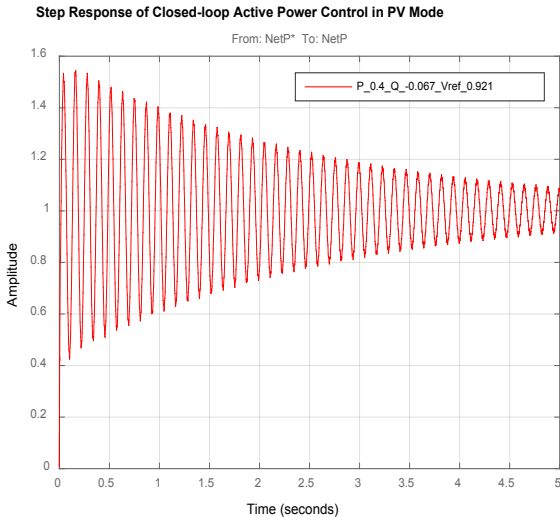
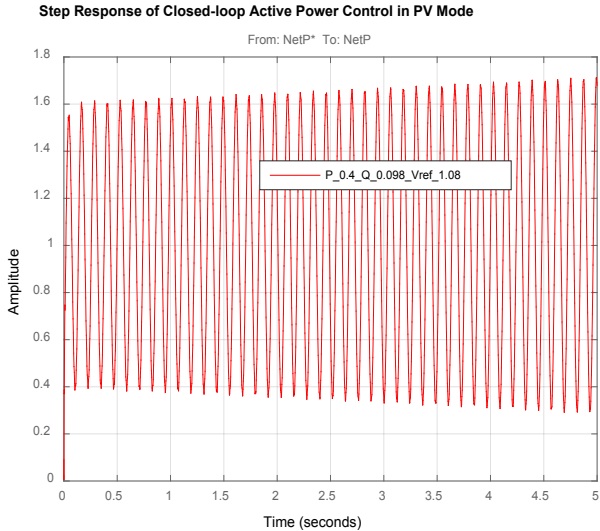
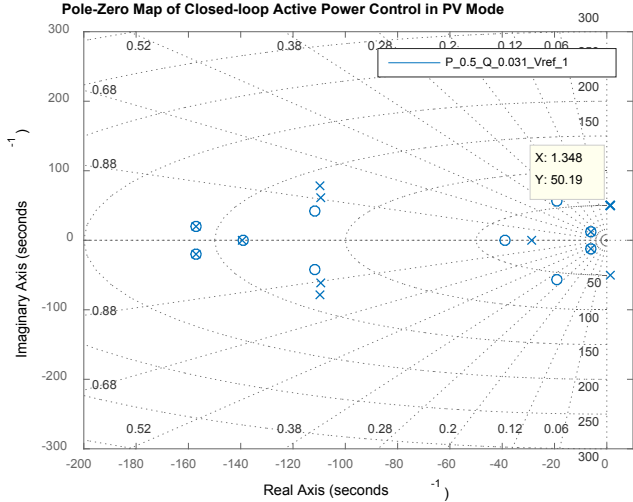
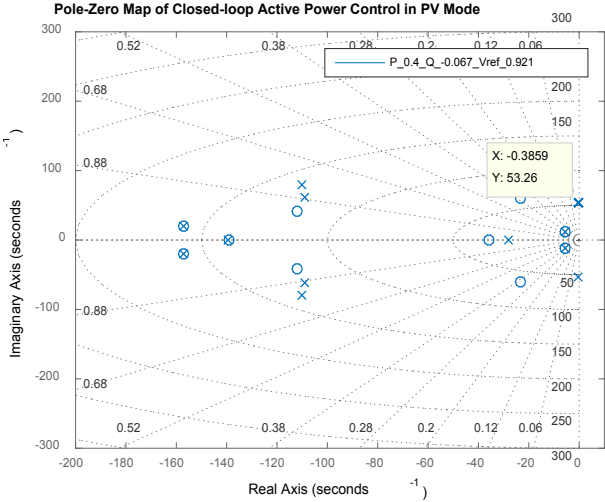
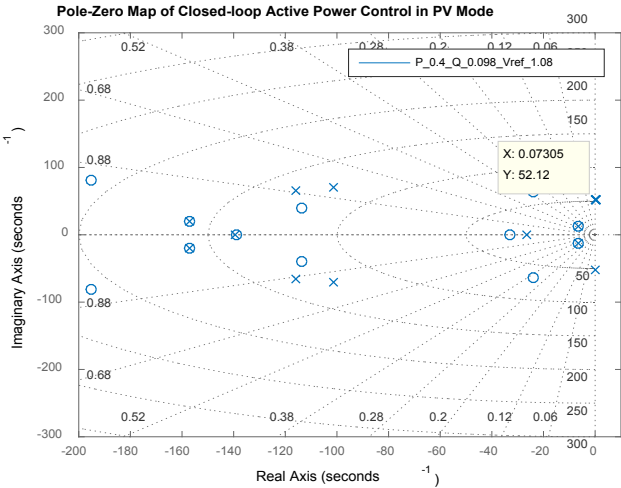
Simulation Scenarios

- Test case 1: 60WTs, $P = 0.4 \cdot P_n$, $V_{ref} = 1.0$ p.u.
 $F_{os} = 8.4$ Hz



Site Oscillation Replication in Simulations (2/2)

Test case 2: $P = 0.4 \cdot P_n$, $V_{ref} = 1.08$, $F_{os} = 8.3\text{Hz}$ Test case 3: $P = 0.4 \cdot P_n$, $V_{ref} = 0.92$, $F_{os} = 8.5\text{Hz}$ Test case 3: $P = 0.5 \cdot P_n$, $V_{ref} = 1.0$, $F_{os} = 8.0\text{Hz}$



Control Tuning for Stabilization of Oscillation

Control Tuning Approach and Robustness Criteria

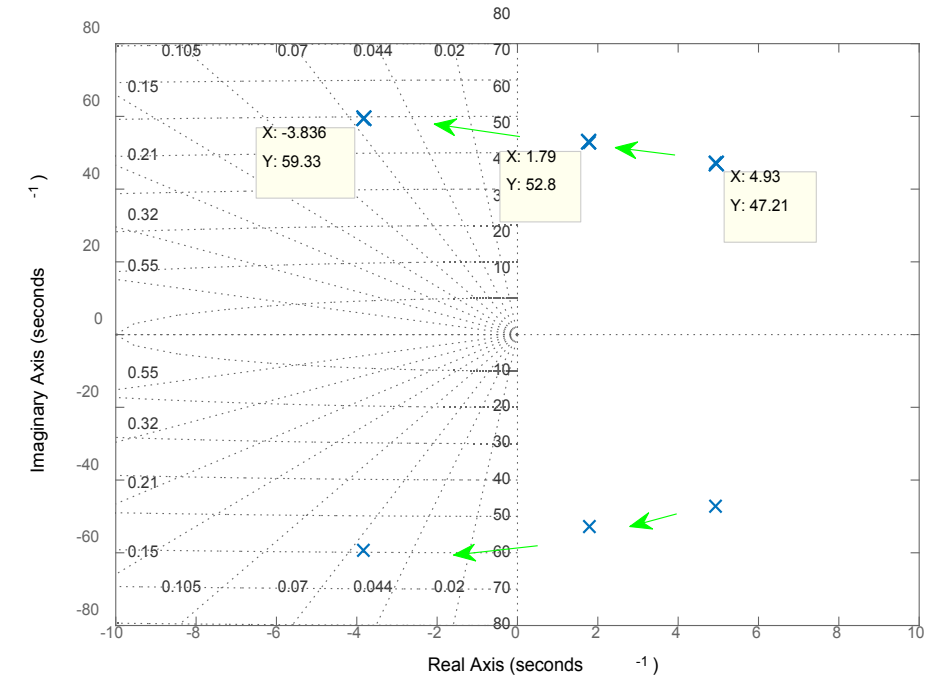
Control Tuning Approach based on relocation of critical poles

- **Rationality:** the LTI system stability depends on if and if only all the poles of state matrix are located in LHP.
- **Objective:** Relocation of unstable poles back in stable region LHP by tuning control parameters.

Robustness Criteria

The robustness criteria is measuring the robustness of a system against external disturbances, expected system changes such as fault level etc.

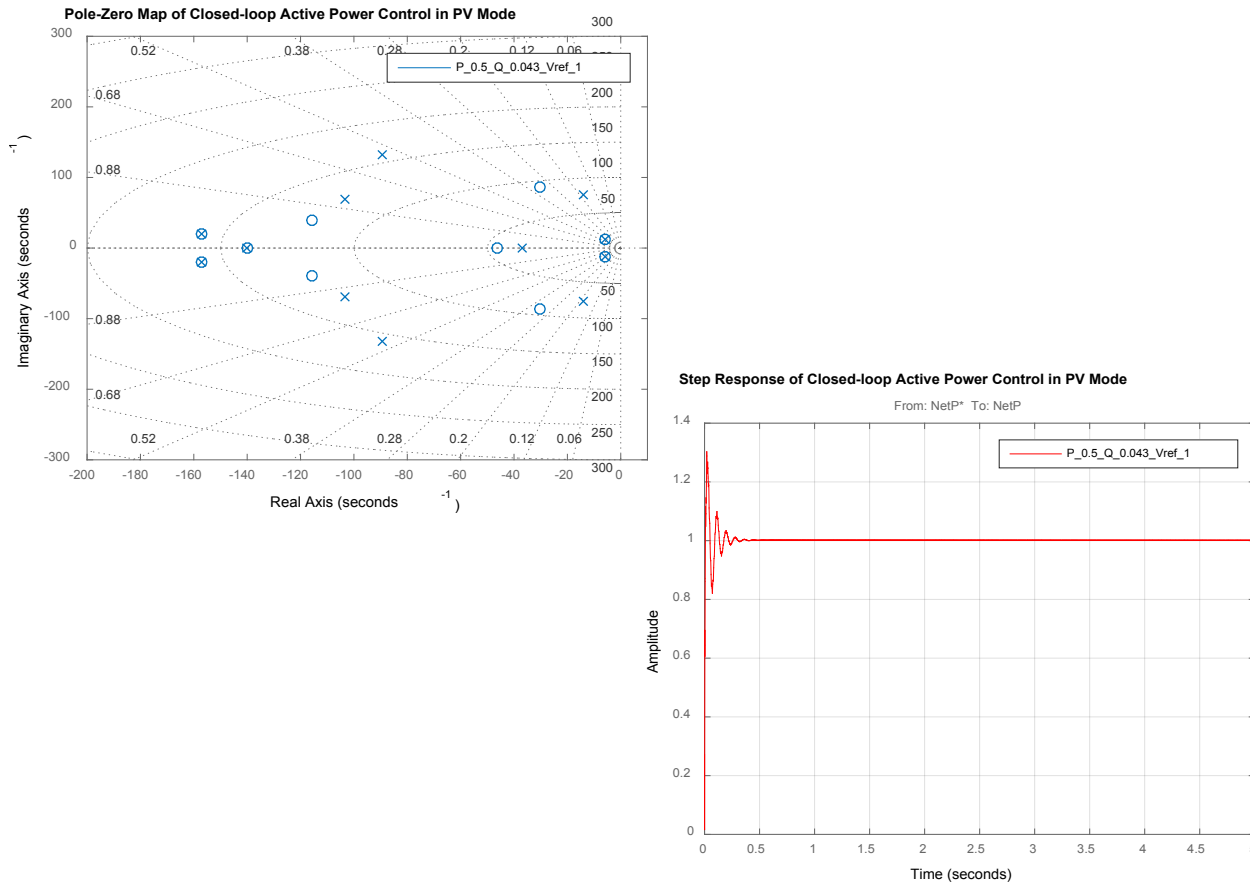
- *Step response overshoot should be less than 35%*
- *Step response setting time should be less than 1s*



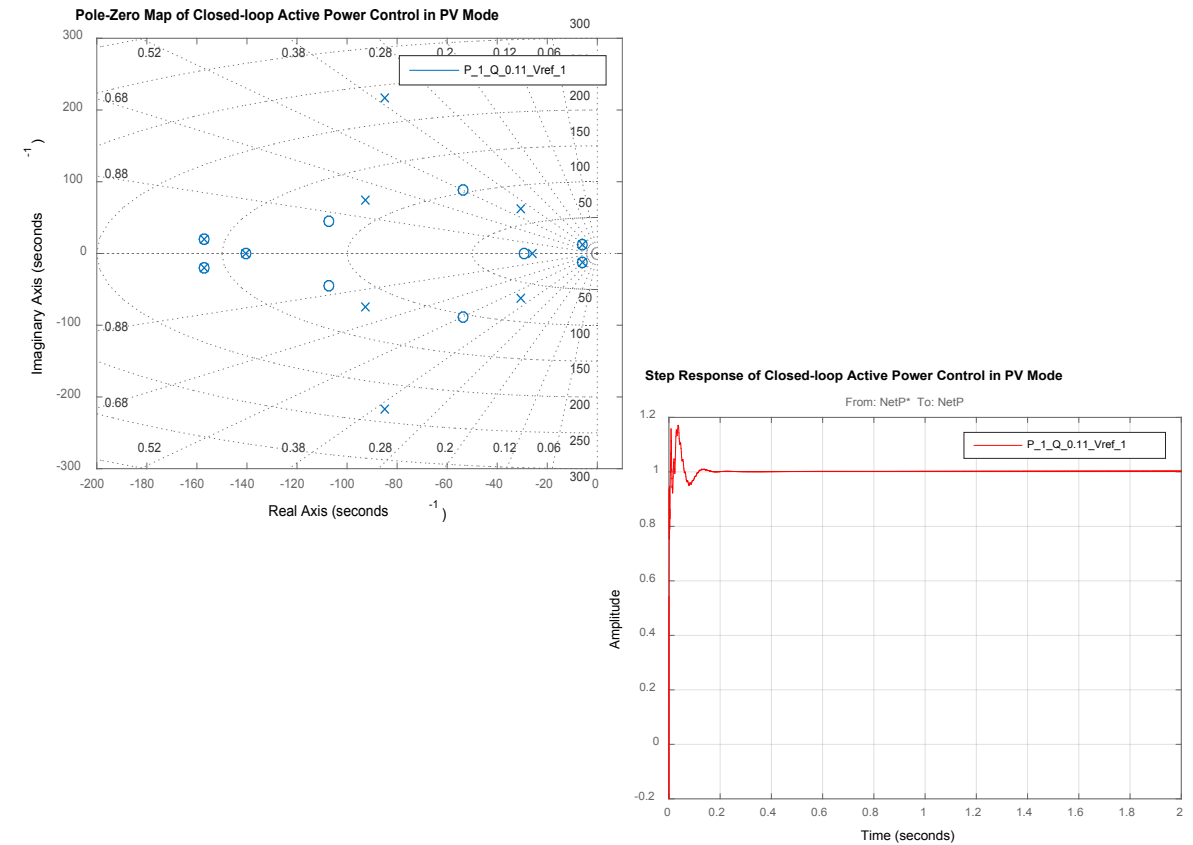
System Performance with Optimized Control

A set of optimized control parameters was identified based on above stability approach and robustness criteria

Test case 1: Single exporting-cable, 67WTs, $P = 0.5 \cdot P_n$, $V_{ref} = 1.0$



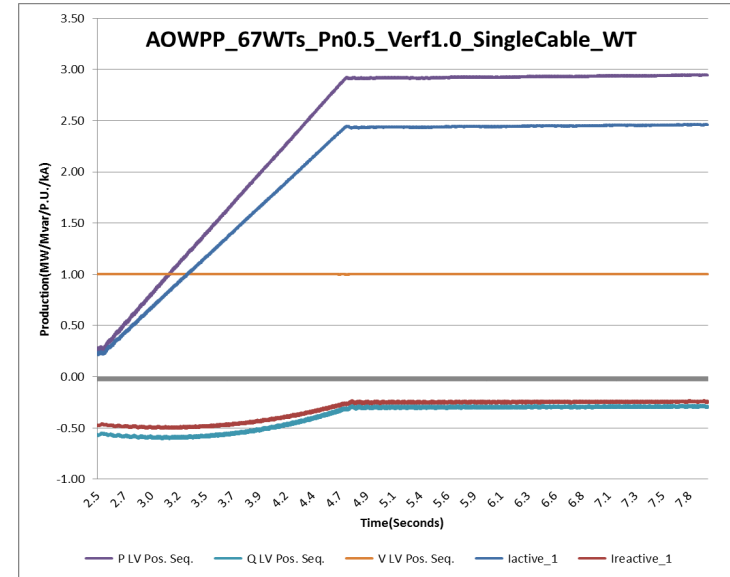
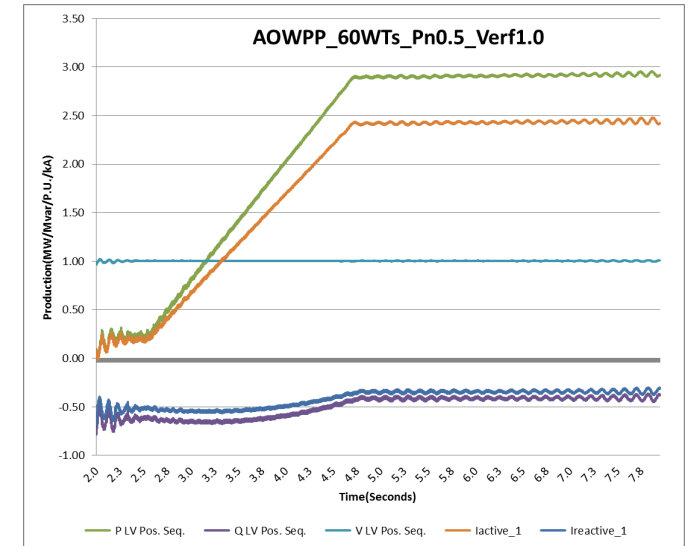
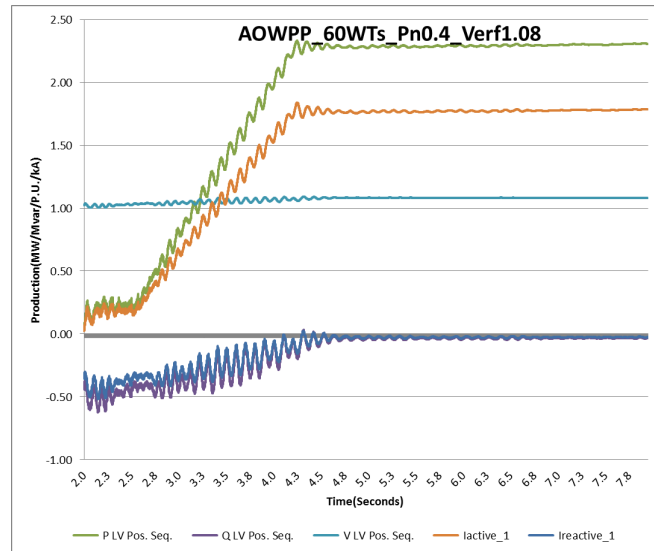
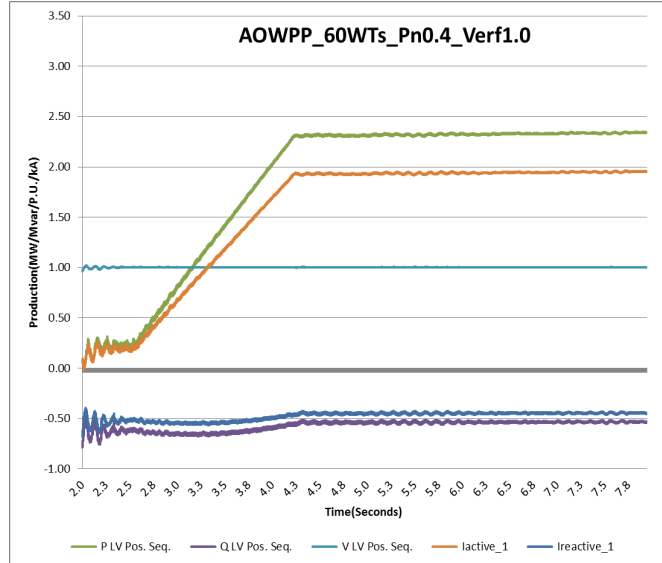
Test case 2: Normal operation, 67WTs, $P = P_n$, $V_{ref} = 1.0$



Benchmarking in PSCAD

Site Oscillation Replication in PSCAD

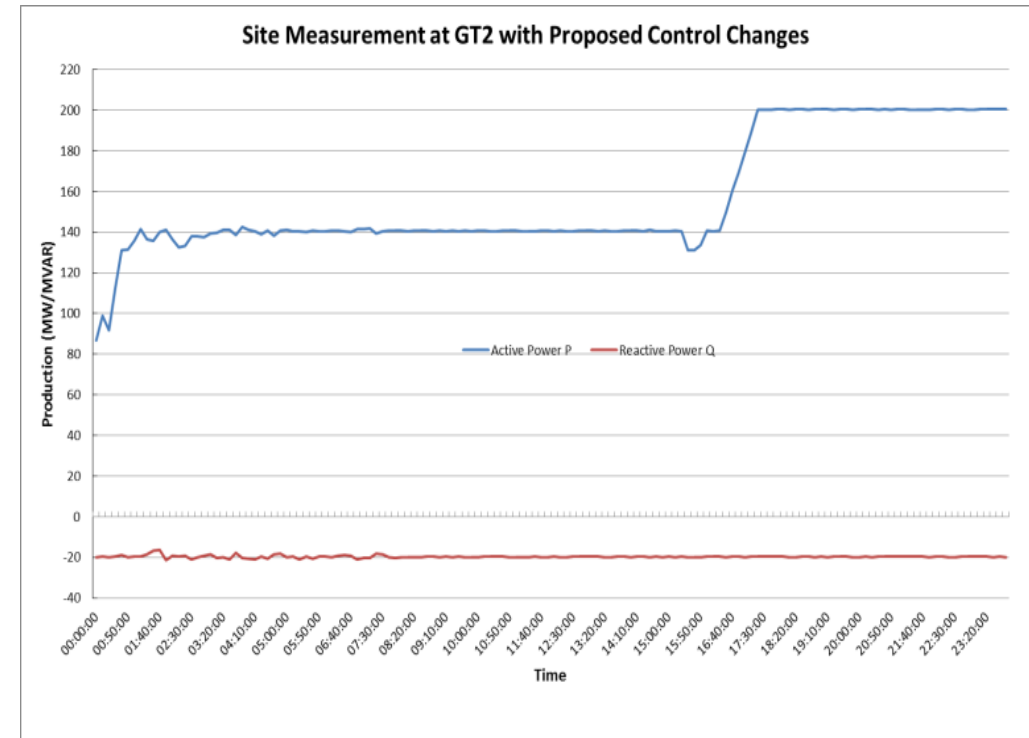
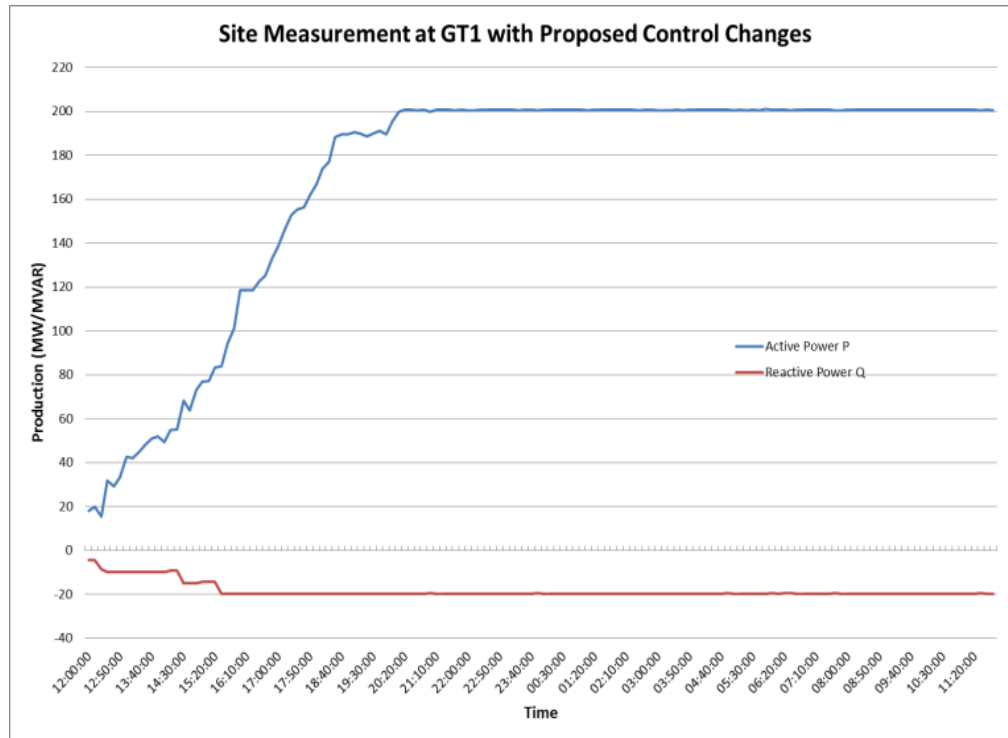
- Full-Order-Model PSCAD consists of the mechanical, electrocal components and corresponding control systems
- PSCAD is able to replicate the site oscillations under similar opeartion conditions as the Eigenvalue-based SSR stability approach
- PSCAD with optimized control shows the sytem oscilaltions have been stablized in max. Power production



Site Validation

Site Validation with Proposed Optimized Control

- The proposed control changes of power converter were applied on site
- Contingency operations were configured once again to verify if the system is stable or not
- Site measurements show the AOWPP is able to run stably with maxim. Production in both contingency operations



Conclusion

Conclusion

- **SSR SRF based simulation modelling has successfully replicated a real site sub-synchronous oscillation**
- **The Eigenvalue-based stability analysis approach has been employed and verified**
- **The control tuning approach based on relocation of critical poles are developed and applied**
- **Robustness criteria are proposed to assess system ability against external disturbances and system changes**
- **Cross-checking in PSCAD was conducted, and very similar results were obtained**
- **Site validation was carried out to verify the system stability with proposed control changes, and therefore has verified the validity of modelling approach, control tuning approach**



Thanks for your attention!

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